RACQUET CLUB OF ANN ARBOR SITE RENOVATIONS SITE PLAN CITY OF ANN ARBOR, WASHTENAW CO., MICHIGAN SITE PLAN SUBMITTAL 3 - 5/15/2015

OWNER/DEVELOPER

RACQUET CLUB OF ANN ARBOR 3010 HICKORY LANE. ANN ARBOR, MI 48108 PH: (734) 216-0579 ATTN: BRENT SCHOMAKER

ANN ARBOR RACQUET CLUB Narrative Description

DEVELOPMENT PROGRAM SUMMARY

The Ann Arbor Racquet Club is a tennis and swim club that began in the mid 1960's and is located at 3010 Hickory lane at the southwest corner of Geddes and Huron Parkway. Facilities at the club include clay and all weather tennis courts, a full size pool, tennis locker rooms, office and pro shop, children's pool, playground amenities and grilling and food vending. The facility is open seasonally during daylight hours only. The original pool and tennis building are 50 years old and lacking modern functionality and accessibility. The tennis building has been particularly problematic in that it has a basement that cannot be utilized due to groundwater flooding. Additionally the building is constructed such that visitor must ascend and descend a half of a flight of stairs to enter and exit the building.

The proposal contained here-in includes the demolition of the existing tennis building and replacing it with a new, single story 3533 SF facility that will be accessible to all. Also included is an addition to the pool building that will facilitate a common, central entry and check in point for all entering and exiting club members as well as new office and laundry facilities. Additional improvements include and addition to the snack shack, patio and pedestrian improvements and storm water detention.

A. Proposed Land Use

The Ann Arbor Racquet Club will continue to operate as a private tennis, swim and recreational facility.

B. Phasing and Construction Cost

- (B.1) Preliminary Phasing: All construction shall be completed in one phase beginning in the fall of 2015 and being completed in the spring of 2016.
- (B.2) Preliminary Cost Estimate: The combined estimated total project construction cost, including utilities, structures, landscaping and site amenities is approximately \$2.5 million.
- 1. <u>Community Analysis</u>
- (a) Impact on Schools
- The project will have no impact on the school system
- (b) Relationship with Neighboring Uses
- The proposal is consistent with the existing use at this site and should present no objection to neighboring uses North of Site: The north side of the site is Geddes Road leading down to the
- Huron River West of Site: Hickory Lane lies west of the site and serves adjacent residential properties that were developed after the club was established. South of Site: Contains the Huron Hills Golf course.
- East of Site: Contains a public ROW for what once was the entrance from Geddes Road onto south bound Huron Parkway. It is now a bike lane.
- (c) Impact on Adjacent Uses

The proposed development will have no negative impact on existing uses around the site and is consistent with the current use.

• Air Quality: The proposal will have no impact on air quality.

(d) Impact of Development Relevant to Various Issues:

- Water Quality: The reconstructed parts of this site will be provided with storm water management facilities in accordance with current standards and discharged in accordance with City of Ann Arbor and Washtenaw County Water Resources Commissioner standards. There currently are no stormwater management facilities on the site at all. Stormwater will be collected from the parking lot through an existing network and then directed into a new underground stormwater tank farm for
- storage and infiltration. • Natural Features: Sheet 1 of the site plan provide a graphic description of the natural features that are found on the site. Natural features on this site consist solely of landmark trees. The area that is proposed for development is almost entirely existing improvements in the form of buildings and pedestrian improvements. The development program concentrates all of the activities in this area thus eliminating any impact to landmark trees.
- Wetlands: The site contains no wetlands.
- Steep Slopes: the site contains no steep slopes. • Floodplains: There are no 100 year floodplains or watercourses that will be impacted by the development.
- Endangered Species or Habitat: None known to exist
- Woodlands: There are no qualifying woodlands on site. • Solid Waste - Solid waste removal will be contracted privately using the existing
- facilities • There are no historical sites, structures or districts impacted by the proposed development
- 1. <u>Site Analysis</u>

(a) Existing Land Use

The existing land zoning is Agricultural while the use of the parcel is recreational. The land has been utilized in this fashion for decades.

(b) Site Conditions

The site is shown in the USDA Soil Conservation Service Soil Survey of Washtenaw County to be primarily Boyer series with 0 to 6% slopes. Site vegetation includes almost exclusively planted trees and shrubs and several native landmark trees that will not be

affected. Topography ranges from 785 USGS down to 769 USGS. Sheet 1 of the Area Plan graphically depicts the site conditions.

- (c) Natural Features Description
 - No endangered species are known to exist on-site. There is no 100-year floodplain on-site.
 - The landmark trees on site are shown on Sheet 1.
 - There are no steep slopes on the site. There are no permanent watercourses on-site
 - There are no wetlands on the site. There are no woodlands on the site.
- (d) Existing Structures

The site contains a managers residence with a detached garage, a pool building a tennis building, a snack shack grill and two barns for storage.

(e) Access Points

Vehicular: The site has access through two entrances off of Hickory Lane and one off Geddes Road. No other connections to adjacent properties are anticipated.

Pedestrian and Bicycle: There are currently no paths or walks along Geddes in front of this location and none are proposed with this project due to safety reasons. The City is planning to install sidewalks along the north side of Geddes Road in 2016, but not will not be installing any on the south side. There are currently no paths proposed on Hickory Lane as there are no paths or sidewalks in the neighborhood.

Associated with a previous site plan administrative amendment in 2008, City Council Resolution R-08-140 waived the sidewalk requirement for site plan petition file AA08-019. This Resolution does not waive the requirement in perpetuity or run with the land, however we are requesting the waiver to continue as the reasons for requesting it have not changed.

(f) Utilities

Water: Water is received from a public main located in Geddes Road. Sanitary Sewer: Sewage drains to a public main located in Huron Parkway

Storm Sewer: Storm sewer will collect and drain stormwater runoff to a new underground storm water detention and infiltration unit on the site.

(g) Drainage

All on-site drainage that is equitable to the new improvements will be detained on-site until it is discharged in accordance with City of Ann Arbor and Washtenaw County Water Resources Commissioner standards. The stormwater discharges to a centeral storm sewer which will divert the flow into an underground detention and infiltration chamber. The proposed drainage system will be completely internal to the site and utilize sheet flow, underground storm sewer and swirl separators that filter the stormwater and release the runoff at a pre-developed rate of discharge.

Traffic Impact

The scope of this project includes the reconstruction of existing facilities only. No new uses or expansion of existing uses is proposed therefore no new trip generation is expected.

GENERAL NOTES:

PER CHAPTER 49, SECTION 4:58 OF THE CITY CODE, "ALL SIDEWALKS ARE TO BE KEPT AND MAINTAINED IN GOOD REPAIR BY THE OWNER OF THE LAND ADJACENT TO AND ABUTTING THE SAME." PRIOR TO ISSUANCE OF THE FINAL CERTIFICATE OF OCCUPANCY FOR THIS SITE, ALL EXISTING SIDEWALKS MUST BE REPAIRED IN ACCORDANCE WITH CITY STANDARDS.

THE CONSTRUCTION COVERED BY THESE PLANS SHALL CONFORM TO THE CITY OF ANN ARBOR PUBLIC SERVICES DEPARTMENT STANDARD SPECIFICATIONS AND DETAILS WHICH ARE INCLUDED BY REFERENCE.

THE OMISSION OF ANY STANDARD DETAILS DOES NOT RELIEVE THE CONTRACTORS OF THEIR OBLIGATION TO CONSTRUCT ITEMS IN COMPLETE ACCORDANCE WITH PUBLIC SERVICES DEPARTMENT STANDARD SPECIFICATIONS.



SCALE: 1'' = 60'





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A PART OF THIS PROJECT. INFORMATION. AND SCHEDULES.	SCALE:	1'' = 30'	CONSULTING I and 3815 Plaza Drive ineers Ann Arbor, Michigan 48108 Phone: 734.995.0299 its Fax 734.995.0599
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BnB		 EROSION EEL (OR EQUAL) TREE PROTECTION FENCE TEMPORARY SECURITY CHAIN-LINK PANEL FENCE ON PEDESTALS (USE PANELS AS GATE) SILT SACK INLET FILTER ON EXISTING INLET SILT SACK INLET FILTER ON NEW INLET IMMEDIATELY AFTER CONSTRUCTION OF INLET PROPOSED BUILDING BUILDING STAGING AREA STORAGE AREA (NO SOILS) SOIL STOCKPILE AREA CONCRETE WASHOUT STRUCTURE DEWATERING FILTER BAG CONSTRUCTION TRAILER LOCATION 	JB OF ANN ARBOR CLIENT ITE PLAN D STAGING PLAN
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The underground utilities shown have been located from field survey information and existing records. The surveyor makes no guarantees that the underground utilities shown comprise all such utilities in the area, either in-service or abandoned. The surveyor further does not warrant that the underground utilities shown are in the exact location indicated. Although the surveyor does certify that they are located as accurately as possible from the information available.

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Stormwater Narrative **Racquet Club of Ann Arbor** May 12, 2015

Ordinance: This project is bound by the Washtenaw County Water Resources Commissioner Rules and Guidelines, Issued August 6, 2014. The regulations require that the greater of the 1-inch storm volume or the increase in the 2-year storm volume be infiltrated, if feasible, and that the 100-year storm runoff be reduced to less than 0.15 cfs/acre. If infiltration is infeasible, an additional 20% penalty is applied to the storage volume required. Additionally, the 1-inch storm must be treated for water quality to remove 80% of total suspended solids.

Portion of Site Modified: If less than 50% of a site is being modified, the portion modified must be fully brought up to standards, and the remainder of the site must be treated for quality. If more than 50% of a site is modified, the full site must be brought up to current standards. This site will be 12.7% modified (0.98 of 7.72 acres), so the modified portion will be infiltrated, with the remainder treated for quality.

General Approach: The site consists of BnB Boyer Loamy Sands, a Type A well-draining soil. However due to current basement flooding issues near the buildings, the project will take the storm water to the north end of the site, near Test Pit 1. Due to the very well draining soils, the project will infiltrate the entire 100-year storm event in less than 48 hours, with the only outlet pipe from the infiltration chambers being an emergency overflow pipe to the existing storm line.

Infiltration Rate: The infiltration test results from Test Pit 1 indicated a 27.75 in/hour infiltration rate. The WCWRC requires a minimum factor of safety of 2, and we are using a factory of safety of 4, to obtain a design infiltration rate of 6.94 in/hr. With this rate the full 4' high chambers can infiltrate the 100-year storm in 6.6 hours.

Outlet Path: Presently, most of the paved portions of the site drain through catch basins into a 6inch storm pipe running from south to north on the site, before tying into the City storm sewer on Huron River Drive. While this pipe is undersized based upon modern design standards, the facility has not faced surface ponding issues due to the generally well-draining soils and the well-established overland flow paths throughout the site. Additionally, portions of the site sheet-flow to the east, south, and north across vegetated surfaces, partially infiltrating into the ground, with the remainder eventually reaching the City's storm sewers in the adjacent roadways.

Infiltration Chamber Design: Due to a desire to preserve landscaping and reduce construction impacts, the infiltration system will be placed underground in chambers, near Test Pit 1. To further reduce site impacts, RTank (or engineer-approved equal) chambers with 93% voids will be used, and the pre-treatment and emergency outlet control with invert at the top of the chamber elevation will also be underground. They are sized to handle the full 100-year storage volume of the disturbed site area, and our calculations indicate that due to infiltration out of the chambers during the storm events, the tank will not overflow when handling the larger stormwater volume routed to them in a 100-year event.

Water Quality Design: Before entering the infiltration chamber, the stormwater will pass through a hydrodynamic separator (Contech CDS or approved equal) sized to handle the pipe capacity leading to it. The hydrodynamic separator will treat the 10-year design storm flow rate (2.8 cfs) to at least the 80% TSS standard, and any remaining solids will be filtered in the soils beneath the infiltration chamber.

Conveyance Systems: New Pipes and swales are designed to convey the 10-year storm without surcharging above the crown of pipe, flowing full, following the calculation methodology in the WCWRC Rules and Guidelines.

Free Release Areas: Certain small areas (0.28 acres) along the edge of the site free-release to the east, west, north, and south, and to the pool, as collecting the water from these areas is difficult. However they are mitigated by taking in 0.40 acres of undisturbed site runoff at Structure R-37. Calculations of the "disturbed area runoff" and of the "infiltrated area runoff" were undertaken to ensure that the stormwater requirements would be exceeded. The project intends to use this trade-off of areas to comply with the regulations.

<u>LEGEND:</u>

LIMITS OF DISTURBANCE MAIN SITE WORK

LIMITS OF DISTURBANCE HICKORY LANE SIDEWALK WORK (EXEMPT FROM STORMWATER MANAGEMENT REUQIREMENTS)

BREAK LINE BETWEEN DETAINED AND FREE RELEASE

42

WATERSHED BOUNDARY FOR CHAMBERS

SUB-WATERSHED BOUNDARY FOR INLET DRAINAGE AREAS

INLET & SUB-WATERSHED NUMBER

ROOF AREA

PAVEMENT AREA

PERMEABLE PAVEMENT AREA

OFFSITE PAVEMENT AREA DRAINING TO CHAMBERS

The underground utilities shown have been located from field survey information and existing records. The surveyor makes no guarantees that the underground utilities shown comprise all such utilities in the area, either in-service or abandoned. The surveyor further does not warrant that the underground utilities shown are in the exact location indicated. Although the surveyor does certify that they are located as accurately as possible from the information available.

				Midw	estern Cons 5/12/2015	sulting
Rational C Values:						_
Soil Type	Roof/Pvmt.	Vegetated	Perm. Paver*	Steep Vegetated (>8%)	Water	
А	0.95	0.20	0.25	0.25	1.00	
В	0.95	0.30	0.35	0.35	1.00	
С	0.95	0.35	0.40	0.40	1.00	
D	0.95	0.50	0.55	0.55	1.00	

* Steep Vegetated C Value used for permeable pavers.

NRCS Soils Type - Entire Site: BNB - Boyer Loamy Sand - Type A Hydrologic Soil Group - 0.60 - 6.00 in/hour infiltration

Inlet #	sft total area	sft roof	sft pvmt.	total imp.	sft perm. Paver	sft veg.	Soil Type	Imp. C	Perm.	Veg. C	CxA	CxA	Area	С
									Paver C		(sft)	(ac)	(ac)	
R-37 (disturbed area)	6,900	0	4976	4,976	72	1,852	А	0.95	0.25	0.20	5,116	0.117	0.158	
R-38	1,310	0	278	278	459	573	A	0.95	0.25	0.20	493	0.011	0.030	
R-40	1,952	0	642	642	384	926	А	0.95	0.25	0.20	891	0.020	0.045	
R-43	5,018	0	1341	1,341	454	3,223	А	0.95	0.25	0.20	2,032	0.047	0.115	
R-45	2,537	0	51	51	0	2,486	А	0.95	0.25	0.20	546	0.013	0.058	
R-46	1,099	0	302	302	0	797	A	0.95	0.25	0.20	446	0.010	0.025	
R-47	1,651	0	915	915	0	736	А	0.95	0.25	0.20	1,016	0.023	0.038	
R-49 (Tennis Bldg.)	3,562	3562	0	3,562	0	0	А	0.95	0.25	0.20	3,384	0.078	0.082	
R-51 (Snack Shack)	812	812	0	812	0	0	A	0.95	0.25	0.20	771	0.018	0.019	
R-53 (Pool Bldg.)	4,433	4433	0	4,433	0	0	A	0.95	0.25	0.20	4,211	0.097	0.102	
East Free	1,163	0	0	0	0	1,163	A	0.95	0.25	0.20	233	0.005	0.027	
South Free	2,421	0	1344	1,344	0	1,077	A	0.95	0.25	0.20	1,492	0.034	0.056	
West Free	1,165	0	182	182	0	983	A	0.95	0.25	0.20	370	0.008	0.027	
North Free	6,637	0	3679	3,679	0	2,958	A	0.95	0.25	0.20	4,087	0.094	0.152	
To Pool Free	1,976	0	1827	1,827	0	149	А	0.95	0.25	0.20	1,765	0.041	0.045	
R-37 - (From Undisturbed)	17,210	740	7723	8,463	0	8,747	А	0.95	0.25	0.20	9,789	0.225	0.395	
Hickory Sidewalk (Exempt)	6,596	0	2190	2,190	0	4,406	A	0.95	0.25	0.20	2,962	0.068	0.151	
Subtotals: A = disturbed are	eas. routed throu	uah detentio	on chamber. B	= disturbed a	areas, free releas	ed. C = ur	ndisturbed a	areas, route	d through ir	nfiltration ch	amber. D	= Total flow	s into Inlet	37

Racquet Club of Ann Arbor - Sub-Watershed Analysis

-	,	5			,			,	5			
A (Dist/Inf)	29,274	8,807	8,505	17,312	1,369	10,593	A	0.95	0.25	0.20	18,907	0.43
B (Dist/Rel)	13,362	0	7,032	7,032	0	6,330	A	0.95	0.25	0.20	7,946	0.18
C (Undist/Inf)	17,210	740	7,723	8,463	0	8,747	A	0.95	0.25	0.20	9,789	0.22
D (Total R-37)	24,110	740	12,699	13,439	72	10,599	A	0.95	0.25	0.20	14,905	0.34
Totals to determine stormw	vater treatmen	t required	: A + B (All di	isturbed area	as)							

A+B (disturbed) 42,636	8,807 1	15,537 24,344	1,369 16,923 A	0.95	0.25	0.20	26,854	0.6
Totale to determine prepaged systems. A L	C (Treating C in	stead of D to allow	for proctical water distribution)					

A+C (proposed) 46,484 9,547 16,228 25,775 1,369 19,340 A 0.95 0.25 0.20 28,697 0.659 1.067 0.62

Proposed stormwater treatment plan:

Because C > B, and infiltration is feasible near C but not by B, the project intends to treat C instead of B as follows:

1) Provide underground storage chambers for the 100-year storm in Area A, near Area A, to release at 0.15 cfs/acre of A 2) Provide underground infiltration chambers for the 2-year storm in Area C, instead of Area A

3) Provide additional storage for Area C, sized for the volume of the 100-year storm in Area B. Release rate will be 0.15 cfs/acre of C.

4) By City Code, public sidewalks are exempt from stormwater management requirements, and they are also off the property on City right-of-way, so the Hickory Sidewalk Area is not included in the project stormwater system.

								Runoff	Formula:		Q =	CIA						
	STERN C	ONSULTI	NG, INC.					· // T · · · ·				475		05		(10	Veen Ote	
3815 P	laza Drive	100				Tune	= 	x/(1+y)	-		x =	175	y=	25		(10	Year Sto	rm Event)
AIIII AI	001, IVII 40 05 0200 I	0100 Eav. (212) (005 0500			туре с		0.013		-	Min time	of conce	ntration	15.00	min			
(313) 9	90-0200, I	rax (313)	990-0099					0.013		-			manon	15.00	111111			
		Drainage	Runoff												Velocity			
		Area	Coeff.		ADD.		Time	Rainfall		Q		Pipe		H.G.	Flowing	Travel	Sewer	Spare
Struc	ture No.	A	С	CxA	CxA	Σ CxA	Т		Q	Inlet	Dia.	Length	Slope	Slope	Full	Time	Capacity	Capac.
From	То	(Acres)					(min.)	(in./hr.)	(cfs)	Here	(in.)	(ft.)	%	%	(ft./sec.)	(min.)	(cfs)	(cfs)
R-31	R-30										6	15	6 48	0.00	7 29	0.03	1 43	1 43
R-34	R-32										12	18	0.40	0.00	3.99	0.00	3 13	3 13
											12		0.11	0.00	0.00	0.00	0.10	0.10
R-36	R-35	0.000	0.00	0.00		0.66	17.31	4 14	2 73	0.00	15	9	0 40	0.18	3 34	0.04	4 10	1.37
R-37	R-36	0.553	0.62	0.34		0.66	16.50	4 22	2.78	1.50	15	164	0.40	0.10	3.34	0.82	4.10	1.31
R-38	R-37	0.030	0.38	0.04		0.32	16.00	4 26	1.35	0.05	12	73	0.52	0.10	3.28	0.02	2.58	1.01
R-39	R-38	0.000	0.00	0.00		0.31	16.05	4.26	1.30	0.00	12	13	0.45	0.13	3.05	0.07	2.40	1.09
R-40	R-39	0.045	0.46	0.02		0.31	15.87	4.28	1.31	0.09	12	34	0.45	0.14	3.05	0.19	2.40	1.09
R-41	R-40	0.000	0.00	0.00	0.10	0.29	15.82	4.29	1.22	0.00	12	9	0.45	0.12	3.05	0.05	2.40	1.17
R-42	R-41	0.000	0.00	0.00	0.03	0.19	15.72	4.30	0.81	0.00	12	19	0.45	0.05	3.05	0.10	2.40	1.59
R-43	R-42	0.115	0.40	0.05		0.16	15.56	4.31	0.69	0.20	12	29	0.45	0.04	3.05	0.16	2.40	1.71
R-44	R-43	0.000	0.00	0.00	0.10	0.11	15.30	4.34	0.50	0.00	12	47	0.45	0.02	3.05	0.26	2.40	1.90
R-45	R-44	0.058	0.22	0.01		0.01	15.00	4.38	0.06	0.06	12	55	0.45	0.00	3.05	0.30	2.40	2.34
D 40	D 40	0.005	0.44	0.01		0.00	45.00	4.07	0.40	0.04	10	05	0.50	0.00	0.00	0.04	0.50	0.40
R-46	R-42	0.025	0.41	0.01		0.03	15.06	4.37	0.12	0.04	12	65	0.50	0.00	3.22	0.34	2.53	2.40
R-50	R-46	0.000	0.00	0.00		0.02	15.04	4.37	0.08	0.00	8	8	2.00	0.00	4.91	0.03	1./1	1.63
R-51	R-50	0.019	0.95	0.02		0.02	15.00	4.38	0.08	0.08	8	11	2.00	0.00	4.91	0.04	1.71	1.63
R-47	R-44	0.038	0.62	0.02		0.02	15.00	4.38	0.10	0.10	12	26	0.50	0.00	3.22	0.13	2.53	2.42
R-48	R-44	0.000	0.00	0.00		0.08	15.02	4.37	0.34	0.00	8	5	2.00	0.08	4.91	0.02	1.71	1.37
R-49	R-48	0.082	0.95	0.08		0.08	15.00	4.38	0.34	0.34	8	5	2.00	0.08	4.91	0.02	1.71	1.37
R-52	R-41	0.000	0.00	0.00		0.10	15.01	4.37	0.42	0.00	8	14	2.00	0.12	4.91	0.05	1.71	1.29
R-53	R-53	0.102	0.95	0.10		0.10	15.00	4.38	0.42	0.42	8	2	2.00	0.12	4.91	0.01	1.71	1.29

STORM DRAINAGE CALCULATION SHEET Racquet Club of Ann Arbor - 14058.00 - 5/15/2015

Please note that based on Manning's equation with an "n" of 0.06 for poor condition natural channel,

A 20' wide, 10% side-sloped swale (1' deep), at 1.0% minimum slope, can handle 8.574 cfs at 0.8' full, and 15.55 cfs at full depth.

No inlet > 2.5 cfs (max is 1.50 cfs at R-37)

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Racquet Club of Ann Arbor Preliminary Detention/Infiltration Calculations - Summary Table Midwestern Consulting, LLC

5/12/2015

Portions of the disturbed site free drain, but portions of undisturbed site flow through the stormwater treatment systems. This table compares the 2-year and 100-year runoff volumes to ensure that the flows actually reaching the stormwater treatment systems are at least as great as the volumes required.

Infiltration Volume Required (Disturbed Area):	4,304	cft	0.099 ac-ft
Actual 2-year Volume (Detained Area):	4,557	cft	0.105 ac-ft
Total 100-year Runoff Required (Disturbed Area):	10,353	cft	0.24 ac-ft
Actual 100-year Volume (Detained Area):	10,978	cft	0.252 ac-ft

Volume Provided:

RTank Chambers are used to conserve space and reduce surface demolition and construction costs.

Elevation

Sizing Calculations Storage Required: Void Ratio of Chambers: RTank Volume Required:	10,353 93% 11,132	cft cft	
Bottom of Chambers:	763.0	Infiltration Tes	at Elevation
Top of Chambers:	767.0	(2.5' under lov	<i>w</i> point of 769.5, 3' under pavement of 770.0)
Height of Chambers	4.0	ft	
Rtank Area Required:	2,783	sft	minimum area required to store stormwater in 4' height.
Check for Infiltration: Infiltration Rate by TP-1 Factor of Safety Design Infiltration Rate	27.75 4 6.94	in/hr in/hr	(WCWRC 2 minimum - also accounting for soils variation) 0.578 ft/hr
Time to Infiltrate	48	hr	
Minimum Volume to Infiltrate per hour	216	cft/hr	
Minimum Infiltration Area	373	sft	minimum infiltration area required.
RTank Area Provided	2,700	sft	
W13 - Storage-Elevation Data			

Basin Storage Information

-	(ft)	(sft)	(cft)	(cft)	(ac-ft)
Bottom of Basin	763	2,800	2,604	2,604	0.06
	764	2,800	2,604	5,208	0.12
	765	2,800	2,604	7,812	0.18
	766	2,800	2,604	10,416	0.24
Top of Basin and Overflow Weir	767	0	0	10,416	0.24
Low Point Ground Elevation	769.5	0	0	10,416	0.24
Storago Volumos					
1" Event	2 201	off	0.05	00 ft	
	2,391		0.05		
2-year Event volume	4,557	CIL	0.10		
Full lank volume	10,353	ctt	0.24	ac-tt	
Infiltration Rate	1,561	cft/hr	0.036	ac-ft/hr	0.43 cfs
Time to infiltrate 1" event	1.5	hr	(<24 hours)		
Time to infiltrate 2-year event	2.9	hr	(<48 hours)		
Tiime to infiltrate 100-year event	6.6	hr	· · · ·		
Storage Elevations					
Elevation for 1" event	763.92	Elevation	0.92	ft. depth	
Elevation for 2-year event	764.75	Elevation	1.75	ft. depth	
Elevation for 100-year event	766.98	Elevation	3.98	ft. depth	

Area

Volume | Cum. Volume |Cum. Volume

Area C Value (ac) 0.158 0.030 0.045 0.115 0.058 0.025 0.038 0.082 0.019 0.102 0.027 0.056 0.027 0.152 0.045 0.395 0.151

4 0.672 0.307 0.395 0.553

16 0.979 0.63

Racquet Club of Ann Arbor Outlet Certification 5/12/2015

Outlet from Chambers:

The infiltration chambers are designed to infiltrate the full 100-year storm into the ground in less than 24 hours. The measured infiltration rate at Test Pit 1 was 27.75 in/hr, and we have applied a factor of safety of 4 (twice the required level) to use a design rate of 6.94 in/hr. This matches the NRCS soils type of BnB Boyer Loamy Sand, a Type A soil.

In case of a failure of the infiltration bed or a storm exceeding the design capacity, and overflow outlet with an invert at the height of the infiltration chamber top has been provided to the existing 6" drainage pipe through the site. Although the 6" pipe is undersized to handle a 10-year storm, the existing site's sandy soils and overland overflow paths have ensured that water ponding on the existing site has not been a problem. The renovations to the site will be reducing the flow through the existing system, and reducing the overland flow off of the site, improving the existing drainage conditions.

Outlet Certification:

Based upon the data and criteria outlined above, I hereby certify that the existing drain is the only reasonably achievable stormwater outlet for the proposed stormwater management system, and that the exiting drain has sufficient capacity to serve as an adequate outlet for the proposed system, without detriment to or diminution of the drainage serve that the existing outlet presently provides.

illeto M

Jeremy Matthei, PE #62010 53590

	(Main Infiltration	Chamber)	0.98 ac			
Rational Method Variables	Cover Type Roofs	Soil Type	Area (sft) 8,807	Area (ac) 0.20	Runoff Coeff. (C) 0.95	(C) (Area) 0.
(for first flush) 0.95 for impervious surfaces	Pavements Perm. Pavers	A A	15,537 1,369	0.36 0.03	0.95 0.25	0. 0.
0.25 for permeable pavers (use "steep vegetated" valu 0.20 for pervious surfaces	e) Landscaping Total	A	16,923 42,636	0.39 0.98	0.20 0.63	0. 0.
			Weighted C	Tota	al - Sum(C)(Area) Area Total rea))/(Area Total)	0. 0.
Pervio NRCS Variables	ous Cover Type Perm. Pavers	Soil Type	Area (sft)	Area (ac) 0.03	Curve Number	(CN) (Area 0.
(for bankfull and 100-year calculations)	Landscaping	A	16,923	0.39	39	0.
(use "Landscaping, Poor Condition, Soil Type A" values of the Landscaping, Good Condition, Soil Type A" values of the Landscaping and Condition and Conditio	ie) Total		18,292	0.42	41	0.
				Tota	al - Sum(C)(Area) Area Total	0. 0.
Impervio	Dus Cover Type	Soil Type	Weighted C	- (Sum(C)(A	rea))/(Area Total)	4 (CN) (Area
NRCS Variables (for bankfull and 100-year calculations)	Roofs Pavements	A A A	8,807 15,537	0.20	98 98	0. 0.
98 for Roofs				-		
98 for Pavements	Total		24,344	0.56	98	0.
			Weighted C	Tota	al - Sum(C)(Area) Area Total rea))/(Area Total)	0. 0. g
W2 - First Flush Runoff Calculations (Vff)				(00(0)()	,	
A. Vff = 1" x 1/12" x 43560 sft/ac x A x C	2,238	cft				
	0.05	ac-ft				
W3 - Pre-Development Bankfull Runoff Calculatio	ons (Vbf-pre)	in				
 A. 2 year / 24 hour storm event. P= B. Pre-Development CN (Cood Court M(code, Turce A Soile)) 	2.30))				
(Good Cover Woods, Type A Solis) C. $S = (1000 / CN) - 10$	23.333	in Nin				
 D. Q = [(P-0.2S)^A2] / [P+0.8S] E. Total Site Area excluding "Self-Crediting" BMPs 	0.000 42,636	sft				
F. Vbf-pre = Q x (1/12) x Area	-	cft <i>ac-ft</i>				
W4 - Pervious Cover Post-Development Bankfull	Runoff Calculatio	ns (Vbf-per-post)				
A. 2 year / 24 hour storm event: P=	2.35	in				
B. Pervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$	41 14.289) in				
 D. Q = [(P-0.2S)²] / [P+0.8S] E. Pervious Cover Area from Worksheet 1 	0.000 18,292) in sft				
F. Vbf-per-post = Q x (1/12) x Area	-	cft <i>ac-ft</i>				
W5 - Impervious Cover Post-Development Bankfu	III Runoff Calculat	ions (Vbf-imp-po	st)			
A. 2 year / 24 hour storm event: P=	2.35	in				
 A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. A = V(D A 20)(21 / UD + 0.001) 	2.35 98 0.204	in in				
 A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. Q = [(P-0.2S)^2] / [P+0.8S] E. Impervious Cover Area from Worksheet 1 	2.35 98 0.204 2.122 24,344	in in sft				
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area	2.35 98 0.204 2.122 24,344 4,304 <i>0.10</i>	in in sft cft <i>ac-ft</i>				
 A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. Q = [(P-0.2S)^2] / [P+0.8S] E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year	2.35 98 0.204 2.122 24,344 4,304 <i>0.10</i> Runoff Calculatio	in in sft cft <i>ac-ft</i> ns (V100-per-pos	t)			
 A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. Q = [(P-0.2S)^2] / [P+0.8S] E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= Deprise Cover 2015 - Minimized and the state of the state o	2.35 98 0.204 2.122 24,344 4,304 <i>0.10</i> Runoff Calculatio 5.11	in in sft cft <i>ac-ft</i> ns (V100-per-pos	t)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$	2.35 98 0.204 2.122 24,344 4,304 <i>0.10</i> Runoff Calculatio 5.11 41 14.289	in in sft cft <i>ac-ft</i> ns (V100-per-pos in	t)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Pervious Cover Area from Worksheet 1	2.35 98 0.204 2.122 24,344 4,304 <i>0.10</i> Runoff Calculatio 5.11 41 14.289 0.307 18,292	in in sft cft <i>ac-ft</i> ns (V100-per-pos in in sft	t)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. $S = (1000 / CN) - 10$ D. $Q = [(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. $S = (1000 / CN) - 10$ D. $Q = [(P-0.2S)^2] / [P+0.8S]$ E. Pervious Cover Area from Worksheet 1 F. V100-per-post = Q x (1/12) x Area	2.35 98 0.204 2.122 24,344 4,304 <i>0.10</i> Runoff Calculatio 5.11 41 14.289 0.307 18,292 467 <i>0.01</i>	in in sft cft <i>ac-ft</i> ns (V100-per-pos in in sft cft <i>ac-ft</i>	t)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Pervious Cover Area from Worksheet 1 F. V100-per-post = Q x (1/12) x Area W7 - Impervious Cover Post-Development 100-Ye	2.35 98 0.204 2.122 24,344 4,304 0.10 Runoff Calculatio 5.11 41 14.289 0.307 18,292 467 0.01 ar Runoff Calculat	in sft cft <i>ac-ft</i> ns (V100-per-pos in in sft cft <i>ac-ft</i> tions (V100-imp-p	t) post)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. $S = (1000 / CN) - 10$ D. $Q = [(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. $S = (1000 / CN) - 10$ D. $Q = [(P-0.2S)^2] / [P+0.8S]$ E. Pervious Cover Area from Worksheet 1 F. V100-per-post = Q x (1/12) x Area W7 - Impervious Cover Post-Development 100-Ye A. 2 year / 24 hour storm event: P=	2.35 98 0.204 2.122 24,344 4,304 0.10 Runoff Calculatio 5.11 41 14.289 0.307 18,292 467 0.01 ar Runoff Calculatio	in sft cft <i>ac-ft</i> ns (V100-per-pos in in sft cft <i>ac-ft</i> tions (V100-imp-p in	t) post)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Pervious Cover Area from Worksheet 1 F. V100-per-post = Q x (1/12) x Area W7 - Impervious Cover Post-Development 100-Ye A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$	2.35 98 0.204 2.122 24,344 4,304 0.10 Runoff Calculatio 5.11 41 14.289 0.307 18,292 467 0.01 ar Runoff Calculat 5.11 98 0.204	in sft cft ac-ft ns (V100-per-pos in in sft cft ac-ft tions (V100-imp-p	t) oost)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Pervious Cover Area from Worksheet 1 F. V100-per-post = Q x (1/12) x Area W7 - Impervious Cover Post-Development 100-Ye A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1	2.35 98 0.204 2.122 24,344 4,304 0.10 Runoff Calculatio 5.11 41 14.289 0.307 18,292 467 0.01 ar Runoff Calculat 5.11 98 0.204 4.873 24,344	in sft cft <i>ac-ft</i> ns (V100-per-pos in in sft cft <i>ac-ft</i> tions (V100-imp-p in in sft	t) bost)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. Q = [(P-0.2S)^2] / [P+0.8S] E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. Q = [(P-0.2S)^2] / [P+0.8S] E. Pervious Cover Area from Worksheet 1 F. V100-per-post = Q x (1/12) x Area W7 - Impervious Cover Post-Development 100-Ye A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. Q = [(P-0.2S)^2] / [P+0.8S] E. Impervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. Q = [(P-0.2S)^2] / [P+0.8S] E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area	2.35 98 0.204 2.122 24,344 4,304 0.10 Runoff Calculatio 5.11 41 14.289 0.307 18,292 467 0.01 ar Runoff Calculat 5.11 98 0.204 4.873 24,344 9,886 0.23	in sft cft ac-ft ns (V100-per-pos in in in sft cft ac-ft tions (V100-imp-p in sft cft ac-ft tions (V100-imp-p	t) post)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. Q = [(P-0.2S)^2] / [P+0.8S] E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. Q = [(P-0.2S)^2] / [P+0.8S] E. Pervious Cover Area from Worksheet 1 F. V100-per-post = Q x (1/12) x Area W7 - Impervious Cover Post-Development 100-Ye A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. Q = [(P-0.2S)^2] / [P+0.8S] E. Impervious Cover CN From Worksheet 1 C. S = (1000 / CN) - 10 D. Q = [(P-0.2S)^2] / [P+0.8S] E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W8 - Time of Concentration (Tc-hrs)	2.35 98 0.204 2.122 24,344 4,304 0.10 Runoff Calculatio 5.11 41 14.289 0.307 18,292 467 0.01 ar Runoff Calculat 5.11 98 0.204 4.873 24,344 9,886 0.23	in sft cft ac-ft ns (V100-per-pos in in sft cft ac-ft tions (V100-imp-p in sft cft ac-ft tions (Childrent to the structure in sft cft ac-ft	t) bost)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^{2}] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^{2}] / [P+0.8S]$ E. Pervious Cover Area from Worksheet 1 F. V100-per-post = Q x (1/12) x Area W7 - Impervious Cover Post-Development 100-Ye A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^{2}] / [P+0.8S]$ E. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^{2}] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W8 - Time of Concentration (Tc-hrs) A. Assume 15-minute minimum time of concentration	2.35 98 0.204 2.122 24,344 4,304 0.10 Runoff Calculatio 5.11 41 14.289 0.307 18,292 467 0.01 ar Runoff Calculat 5.11 98 0.204 4.873 24,344 9,886 0.23	in sft cft ac-ft ns (V100-per-pos in in sft cft ac-ft tions (V100-imp-p in sft cft ac-ft tions (V100-imp-p	t) bost)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Pervious Cover Area from Worksheet 1 F. V100-per-post = Q x (1/12) x Area W7 - Impervious Cover Post-Development 100-Ye A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover CN From Worksheet 1 F. V5 = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W8 - Time of Concentration (Tc-hrs) A. Assume 15-minute minimum time of concentration	2.35 98 0.204 2.122 24,344 4,304 0.10 Runoff Calculatio 5.11 41 14.289 0.307 18,292 467 0.01 ar Runoff Calculat 5.11 98 0.204 4.873 24,344 9,886 0.23	in sft cft ac-ft ns (V100-per-pos in in in sft cft ac-ft tions (V100-imp-p in sft cft ac-ft tions (V100-imp-p in sft cft ac-ft	t) Dost)			
A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover Area from Worksheet 1 F. Vbf-imp-post = Q x (1/12) x Area W6 - Pervious Cover Post-Development 100-Year A. 100 year / 24 hour storm event: P= B. Pervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Pervious Cover Area from Worksheet 1 F. V100-per-post = Q x (1/12) x Area W7 - Impervious Cover Post-Development 100-Ye A. 2 year / 24 hour storm event: P= B. Impervious Cover CN From Worksheet 1 C. S = $(1000 / CN) - 10$ D. Q = $[(P-0.2S)^2] / [P+0.8S]$ E. Impervious Cover CN From Worksheet 1 F. V100-per-post = Q x (1/12) x Area W8 - Time of Concentration (Tc-hrs) A. Assume 15-minute minimum time of concentration	2.35 98 0.204 2.122 24,344 4,304 0.10 Runoff Calculatio 5.11 41 14.289 0.307 18,292 467 0.01 ar Runoff Calculat 5.11 98 0.204 4.873 24,344 9,886 0.23	in sft cft ac-ft ns (V100-per-pos in in in in sft cft ac-ft tions (V100-imp-p in sft cft ac-ft tions (V100-imp-p in hr	t) post)			

W9 - Runoff Summary & On-Site Infiltration Requirement	W3 - Pre-Development Bankfull Runoff Calculations (Vbf-pre)	
A. Summary from Previous Worksheets First Flush Volume (Vff)2,238 cft0.05 ac-ft	A. 2 year / 24 hour storm event: P= 2.35 in 30	
Pre-Development Bankfull Runoff Volume (Vbf-pre) - cft - ac-ft	(Good Cover Woods, Type A Soils) C = S = (1000 / CN) - 10 $23 333 in$	Drive
Pervious Cover Post-Development Bankfull Volume (Vbf-per-post) - cft - ac-ft Impervious Cover Post-Development Bankfull Volume (Vbf-imp-post) 4,304 cft 0.10 ac-ft	D. $Q = [(P-0.2S)^2] / [P+0.8S]$ E. Total Site Area excluding "Self-Crediting" BMPs 46,484 sft	aza [34.99
Potrieur Cover Reet Development 100 Year Volume (V100 per peet)	F. Vbf-pre = Q x (1/12) x Area - cft - ac-ft	LS PL Arb
Pervious Cover Post-Development 100-Year Volume (V100-per-post) 467 cm 0.01 ac-m Impervious Cover Post-Development 100-Year Volume (V100-imp-post) 9,886 cft 0.23 ac-ft Total 100-Year Volume (V100) 10.353 cft 0.24 ac-ft	W4 - Pervious Cover Post-Development Bankfull Runoff Calculations (Vbf-per-post)	381 Anr
	A. 2 year / 24 hour storm event: P= 2.35 in	and
B. Determine Onsite Infiltration Requirement Subtract the Pre-Development Bankfull from the Post-Development Bankfull Volume	B. Pervious Cover CN From Worksheet 1 41 C. S = (1000 / CN) - 10 14.440 in	ental Engir
Total Post-Development Bankfull Volume (Vbf-post)4,304cft0.10ac-ftPre-Development Bankfull Runoff Volume (Vbf-pre)-cft-ac-ft	D. $Q = [(P-0.2S)^{n}2] / [P+0.8S]$ E. Pervious Cover Area from Worksheet 1 20,709 sft E. Vide per peet = Q x (1/12) x Area	surve Surve
Bankfull Volume Difference 4,304 cft 0.10 ac-ft	F. VD-per-post = Q x (1/12) x Area - ch - $ac-ft$	Envi sportc
Compare to First Flush Volume (Vff) 2,238 cft 0.05 ac-ft	W5 - Impervious Cover Post-Development Bankfull Runoff Calculations (Vbf-imp-post)	Civil, Civil, Plan
Greater of Bankfull Volume or First Flush Volume 4,304 cft 0.10 ac-ft To be Infiltrated	A. 2 year / 24 hour storm event: P= 2.35 in B. Impervious Cover CN From Worksheet 1 98	
W10 - Detention/Retention Requirement	C. $S = (1000 / CN) - 10$ 0.204 inD. $Q = [(P-0.2S)^2] / [P+0.8S]$ 2.122 in	
Detention $A = Op = 238.6 \text{ Tc}^{0.0} 82$ 743.63 cfs/(in x sq. mi)	E. Impervious Cover Area from Worksheet 125,775 sftF. Vbf-imp-post = Q x (1/12) x Area4,557 cft	
B. Total Site Area excluding "Self-Crediting" BMPs 0.98 ac C. Q100 = Q100-per + Q100-imp 5.180 in	0.10 ac-ft	
(from W6 and W7, respectively) D. Peak Flow (PF) = $Qp \times Q100 \times Area / 640$ 5.89 cfs	W6 - Pervious Cover Post-Development 100-Year Runoff Calculations (V100-per-post)	
E. Delta = PF - 0.15 x Area (ac) 5.74 cfs [0.15 x Area (ac)] 0.15 cfs	A. 100 year / 24 hour storm event: P= 5.11 in B. Pervious Cover CN From Worksheet 1 41	
F. Vdet = Delta / PF x V100 - Vinf (5,319) cft (0.12) ac-ft Required Detention (All Runoff is infiltrated)	C. $S = (1000 / CN) - 10$ D. $Q = [(P-0.2S)^2] / [P+0.8S]$ D. $Q = [(P-$	ROR
Retention	E. Pervious Cover Area from Worksheet 1 $20,709$ sft F. V100-per-post = Q x (1/12) x Area 511 cft 0.01 cs ft	N AF
A. Vret = 2 x V100 20,706 cft 0.48 ac-ft	u.ur au-it W7 - Impervious Cover Post-Development 100-Year Runoff Calculations (\/100-imp-post))F AN ANE 481(ER
W11 - Determine Applicable BMPs and Associated Volume Credits	A. 2 year / 24 hour storm event: P= 511 in	UB C VY L/ MI MAKE
Proposed BMP Area Stor. Vol. Ave Inf. Rate Inf. Storm Total Red.	B. Impervious Cover CN From Worksheet 1 98 C. S = (1000 / CN) - 10 0.204 in	LT CL ICKOL ICKOL SCHC
(sft) (cft) (in/hr) (cft) Infiltration Chambers 2,700 10,353 6.9 9,366 19,719	D. Q = [(P-0.2S) ²] / [P+0.8S] 4.873 in E. Impervious Cover Area from Worksheet 1 25,775 sft	LIEN CQUE N AR ENT
(Area conservatively taken at bottom of pond) Average infiltration rate at Test Pit 10 (pond location) is 14 in/hr, FS of 2 is 7 in/hr. 3.0in/hr is used here to be conservative.	F. Vbf-imp-post = Q x (1/12) x Area 10,467 cft 0.24 ac-ft	AN C C BR
Total Volume Reduction Credit by Proposed Structural BMPs 19,719 cft	W8 - Time of Concentration (Tc-hrs)	
Runoff Volume Infiltration Requirement (Vinf) from Worksheet 9 4,304 cft Runoff Volume Credit 15,415 cft	A. Assume 15-minute minimum time of concentration 0.25 hr	ō
Minimum Surface Area Check		
Contributing Total Surface 42,636 sft	W9 - Runoff Summary & On-Site Infiltration Requirement	
Total Surface Ratio 15.8	A. Summary from Previous Worksneets First Flush Volume (Vff) 2,391 cft 0.05 ac-ft	
W12 - Natural Features Inventory	Pre-Development Bankfull Runoff Volume (Vbf-pre) - cft - ac-ft - ac-ft - ac-ft	
Existing Natural Resources Mapped Total Area Protected Area (ac) (ac)	Impervious Cover Post-Development Bankfull Volume (Vbf-imp-post)4,557 cft0.10 ac-ftTotal BF Volume (Vbf-post)4.557 cft0.10 ac-ft	A
Wetlands Yes 0.00 0.00 Woodlands Yes 0.00 0.00	Pervious Cover Post-Development 100-Year Volume (V100-per-post) 511 cft 0.01 ac-ft	
Total Existing 0.00 0.00	Impervious Cover Post-Development 100-Year Volume (V100-imp-post)10,467 cft0.24 ac-ftTotal 100-Year Volume (V100)10,978 cft0.25 ac-ft	
Racquet Club of Ann Arbor Preliminary Detention/Infiltration Calculations - Detained Area	B. Determine Onsite inflitration Requirement Subtract the Pre-Development Bankfull from the Post-Development Bankfull Volume	
5/12/2015	Pre-Development Bankfull Runoff Volume (Vbf-pre) - cft - ac-ft Bankfull Volume Difference 4,557 cft 0.10 ac-ft	5
Total Disturbed Area Calculations (to Determine Actual Flow Rates and Volumes to Chambers)	Compare to First Flush Volume (Vff) 2.391 cft 0.05 ac-ft	
W1 - Determining Post-Development Cover Types, Areas, Curve Numbers, and Runoff Coefficients	Greater of Bankfull Volume or First Flush Volume 0.10 ac-ft 0.10 ac-ft	
Total Site Area (Proposed Detained Area) 1.07 ac Total Site Area Excluding "Self-Crediting" BMPs* (Main Detention Basin) 1.07 ac	To be Infiltrated	
* Used for remainder of calculations below	W10 - Detention/Retention Requirement	
Rational Method VariablesCover TypeSoil TypeArea (stt)Area (ac)Runoff Coeff. (C)(C) (Area)Ref red finablesRoofsA9,5470.220.950.21(for finat finable)RememberA16.2290.950.25	Detention A. Qp = 238.6 Tc^-0.82 743.63 cfs/(in x sq. mi) B. Tatal Site Area evaluating "Self Crediting" BMDs 107 cs	A
(for first flush) Pavements A 16,228 0.37 0.95 0.35 0.95 for impervious surfaces Perm. Pavers A 1,369 0.03 0.25 0.01 0.25 for permechle pavers (use "steep vegeteted" velue) Landscapping A 19,340 0.44 0.30 0.09	B. Total Site Area excluding "Self-Crediting" BMPS 1.07 ac C. Q100 = Q100-per + Q100-imp 5.169 in (from)/(6 and)/(7, respectively)	
0.25 for pervious surfacesCalloscapingA19,5400.440.200.090.20 for pervious surfacesTotal46,4841.070.620.66	D. Peak Flow (PF) = Qp x Q100 x Area / 640 6.41 cfs	
Total - Sum(C)(Area) 0.66 Area Total 1.07 ac	[0.15 x Area (ac)] F. Vdet = Delta / PF x V100 - Vinf (4.457.50) cft (0.10) ac-ft	
Weighted C - (Sum(C)(Area))/(Area Total) 0.62 ac	Required Detention	11
PerviousCover TypeSoil TypeArea (sft)Area (ac)Curve Number(CN) (Area)NRCS VariablesPerm. PaversA1,3690.03680.02	Retention 21,956 cft 0.50 ac-ft	
(for bankfull and 100-year calculations) Landscaping A 19,340 0.44 39 0.17		
68 for Permeable Pavers, Soil Type A	W11 - Determine Applicable BMPs and Associated Volume Credits 6-hour	15
39 for Landscaping, Good Condition, Soil Type ATotal20,7090.48410.19	Proposed BMP Area Stor. Vol. Ave Inf. Rate Inf. Storm Total Red. (sft) (cft) (in/hr) (cft) (cft) (cft)	15/20 J B ·
Total - Sum(C)(Area)0.19Area Total0.48	Initiation Champers 2,700 10,353 6.9 9,366 19,719 (Area conservatively taken at bottom of pond) Average infiltration rate at Test Bit 10 (read leastion) is 11 in (hr. 50 of 2 i	TE: 5/ IEET 1 DD: WA CH: SW CH: SW CH: CH: CH: CH: CH: CH: CH: CH: CH: CH:
Weighted C - (Sum(C)(Area))/(Area Total) 40.9	Total Volume Reduction Credit by Proposed Structural RMPs	E CA
Impervious Cover Type Soil Type Area (stt) Area (ac) Curve Number (CN) (Area) NRCS Variables Roofs A 9,547 0.22 98 0.21 (for bankfull and 100-year calculations) Roometric A 16,222 0.37 0.0 0.37	Runoff Volume Infiltration Requirement (Vinf) from Worksheet 9 4,557 cft Runoff Volume Credit 15.162 cft	<u>/. DAT</u>
Partner Partner A 16,228 U.37 98 U.37 98 for Roofs 98 98 0.37 98 0.37	Minimum Surface Area Check	REV.
98 for Pavements Total 25 775 0.50 0.92 0.50	Contributing Impervious Surface 25,775 sft Contributing Total Surface 46.484 sft	
Total - Sum(C)(Area) 0.58	Impervious Surface Ratio9.5 Type A soils at 6.9"/hour drain quickly.Total Surface Ratio17.2	
Area Total0.50Weighted C - (Sum(C)(Area))/(Area Total)98.0		02
	W12 - Natural Features Inventory	 4
W2 - First Flush Runoff Calculations (Vff)	Existing Natural Resources Mapped Total Area Protected Area (ac) (ac)	
A. Vff = 1" x 1/12" x 43560 sft/ac x A x C 2,391 cft 0.05 ac-ft	WetlandsYes0.000.00WoodlandsYes0.000.00Total Evicting0.000.00	No.
		JOE

WETLAND SEED MIX "B" (JF New Wetland Edge & Annual/Perennial Forbs Mixes, or equal)

For Use in Bioswale/Rain Gardens

Scientific Name Carex lurida Carex sp. Carex vulpinoidea Eleocharis palustris major Elymus canadensis Glyceria striata Leersia oryzoides Scirpus atrovirens Scirpus pungens Scirpus validus creber Avena sativa Lolium multiflorum Actinomeris alternifolia Agalinis tenuifolia Alisma subcordatum Asclepias incarnata Aster simplex Bidens sp. Cassia hebecarpa Eupatorium perfoliatum Helenium autumnale lris virginica shrevei Lobelia siphilitica Mirnulus ringens Rudbeckia laciniata Verbena hastata Vernonia sp. Cassia fasciculata Coreopsis lanceolata Lupinus perennis Monarda fistulosa Ratibida pinnata Rudbeckia hirta Cosmos bipinnatus Gaillardia pulchella Papaver rhoeas

Common Name Bottlebrush Sedge Sedge Brown Fox Sedge Great Spike Rush Canada Wild Rye Fowl Manna Grass Rice Cut Grass Dark Green Rush Chairmaker's Rush Great Bulrush (softstem) Seed Oats Annual Rye Wingstem Slender False Foxglove Common Water Plantain Swamp Milkweed Panicled Aster Bidens Wild Senna Common Boneset Sneezeweed Blue Flag Iris Great Blue Lobelia Monkey Flower Wild Golden Glow Blue Vervain Ironweed Partridge Pea Sand Coreopsis Flowerwild Lupine Wild Bergamot Yellow Coneflower Black-eyed Susan Annual Cosmo

Blanket Flower

Annual Corn Poppy

- 6' HIGH OPAQUE PRIVACY FENCE (EX)

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Know what's **below**.

Call before you dig.

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LANDSCAPE REQUIREMENTS:

Provided/existing.

Note applicable.

daylight in the morning.

- VII. TREE MITIGATION: Not applicable.
- VIII. NATURAL FEATURES:
- Statement of Natural Features Impacts is shown on Sheet 2.

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CONSTRUCTION SEQUENCE	AUG	15	SEP	15	OCT	15	NC	DV 15	5 [DEC	15	JAI	V 16	F	ΈB	16	MA	٨R	16	AP	R 1	6	MAY	16	JU	N 16
FINALIZE PERMITS AND HOLD PRE-GRADING MEETING WITH THE CITY OF ANN ARBOR																										
FACILITY CLOSED TO PUBLIC USE																					i i i i i i i i i i i i i i i i i i i					
INSTALL MEASURES AND MAINTAIN SOIL EROSION																										
DEMOLISH EXISTING BUILDINGS AND							\square		T										Π		\square			\square	\square	
INSTALL STORMWATER MANAGEMENT SYSTEM AND HYDRANT LEAD EXTENSION									╈	\square				t					\square							
RESTORE PAVEMENT AND LANDSCAPING IN PARKING LOT AREA																										
ROUGH GRADE SITE									Τ					Γ					Π		Π	\square				
CONSTRUCT BUILDING FOOTINGS									Т					Γ					Π		\square					
CONSTRUCT UTILITY SERVICES AND GRADE SITE ADJACENT TO BUILDINGS														T												
CONSTRUCT BUILDING STRUCTURE AND SHELL																										
CONSTRUCT BUILDING INTERIOR																										
FINE GRADE SITE, INSTALL FENCES, PAVEMENTS, AND_TRELLISES																										
INSTALL LANDSCAPE																										
PROJECT CLOSEOUT AND MISC. CLEANUP																										
IMPLICATIONS OF SAID MAINTENANCE CLUB MANAGEMENT STAFF.	WILL	BE	ADE	RE	SSED) B,	Y TH	HE F	RAC	QUI	ΕT															
CONSTRUCTION SEQUENCE:																										
 OBTAIN SOIL EROSION AND SEDIMENT FROM THE CITY OF ANN ARBOR. TO INSPECT SITE ONCE A WEEK AN PRECIPITATION EVENT. MAINTAIN V SCHEDULE AND ATTEND A SOIL ER PRE-GRADING MEETING WITH THE C MARK TREES AND BRUSHFOR REMC CLOSE FACILITY TO THE PUBLIC ON CLEAR BRUSH AND TREES WHERE IN INSTALL TREE PROTECTION FENCE, FILTER SILT SACKS, AND OTHER SE EROSION CONTROL PLAN FOR FURT 	NTAT CERT ID IM VRITT OSIOI CITY VAL I LAE NDIC SITE SSC [HEP	ION IFIEE EN N AI OF ANE 3OR ATE SE(DEVI	CON MD IATE REP(ND S ANN DAY DAY O, A CURI CES.	TRO EQ ILY DRT DRT DRT C EDI AR OTE () EDI () 2 BO () EDI () 2 BO () 5 C	DL, A STC FOL S ON BOR BOR CTIC 015. VE S FENC EE [ND RM OW S TAT ON. TUN E, DEM	GR WA ING ITE. ION VPS SILT	ADII TER EA CO CO ONI FE	NG OF CH NTF	PEF PER ROL E, I	RMIT ATC NLE AN	r DR T														
 PROTECTION. 7. REMOVE PAVEMENT, STUMPS, AND 8. STRIP TOPSOIL AND STOCKPILE ON 9. CONSTRUCT STORMWATER MANAGEN INSTALL INLET FILTER SILT SACKS 	SITE – SITE /ENT IN AI	STF STF SYS L N	AILS RUCT R R STEN EW	URE EUS I IN	ES, N SE. PAI ETS	VHE RKII AS	RE NG L SOC	INDI LOT	CA ⁻ AR	TED REA. THE	> EY ,	ARE	-						SI	TAPLE	ES	Γ	STRA	W BAL	Ē	BINI
CONSTRUCTED. 10.EXTEND HYDRANT LEAD. 11.INSTALL COMMUNICATIONS CONDUCT	IN F	PARI	KING		τ Δι	۶FΔ												(2 PER	BAL	E)		- 10	mil PL	ASTIC	LINING ERIAL
12. WHILE PARKING LOT UTILITY WORK REMOVE UTILITIES WHERE INDICATED	S IS I S ON	N P RE	ROG MOV/	RES	SS, C PLA	NSC	ONN	IECT	Ā	ND											ţ	K	e::			
13. WHILE PARKING LOT UTILITY WORK WHERE INDICATED ON REMOVALS P	IS IN LAN	i pr ANC	OGR AR	ESS CHI	S, DE TECT	MÖ UR/	LISH AL F	I ST PLAP	RU NS.	СТИ	IRES	5							WO		R		S		ON B- SCAL	B

14. WHILE PARKING LOT UTILITY WORK IS IN PROGRESS, ROUGH GRADE SITE NEAR BUILDINGS.

15. RESTORE PAVEMENT IN PARKING LOT AREA, AS SOON AS POSSIBLE, IN THE FALL OF 2015. 16. RESTORE LANDSCAPE IN PARKING LOT AREA, WITHIN 5 DAYS OF THE FINAL

EARTH CHANGE, AS SOON AS POSSIBLE. IN THE FALL OF 2015. 17. INSTALL SANITARY SEWER AND STORM SEWER NEAR BUILDINGS. INSTALL INLET FILTER SILT SACKS ON ALL NEW INLETS AS SOON AS THEY ARE

CONSTRUCTED. 18. AFTER STORMWATER SYSTEM IS OPERATIONAL, OBTAIN BUILDING PERMITS AND INSTALL BUILDING FOOTINGS. 19. INSTALL REMAINDER OF SITE UTILITIES NEAR BUILDINGS, AND GRADE SITE.

20.CONSTRUCT BUILDING STRUCTURE AND SHELL.

21. CONSTRUCT BUILDING INTERIOR. 22.IN EARLY SPRING 2016, CONSTRUCT SITE PAVEMENTS, FENCES, AND

TRELLISES. 23.PLACE TOPSOIL AND LANDSCAPE SITE. ALL SOILS MUST BE LANDSCAPED (WITH ALL PERMANENT SESC CONTROLS) WITHIN FIVE DAYS OF THE FINAL ÈARTH CHANGE. 24.CLEAN UP SITE.

25.0PEN FACILITY TO THE PUBLIC ON MEMORIAL DAY, 2016.

26.MAINTAIN ALL SESC DEVICES UNTIL VEGETATION IS FULLY ESTABLISHED, THEN REMOVE TEMPORARY SESC DEVICES. 27.CLOSE OUT SITE PERMITS.

CONCRETE WA NOT TO SCAL

MAINTENANCE REQUIREMENTS

1. ALL SILT FENCE SHALL BE MAINTAINED THROUGHOUT THE DURATION OF THE PROJECT. IF AT ANY TIME THE DEPTH OF SILT AND SEDIMENT COMES TO WITHIN 12" OF THE TOP OF ANY SILT FENCE, ALL SILT AND SEDIMENT SHALL BE REMOVED TO ORIGINAL GRADE.

2. ALL TEMPORARY GRAVEL FILTERS SHOULD BE ADJUSTED AS TO LOCATION PER ACTUAL FIELD CONDITIONS. THE REMOVAL OF TRAPPED SEDIMENT AND THE CLEANOUT OR REPLACEMENT OF CLOGGED STONE MAY BE NECESSARY AFTER EACH STORM EVENT DURING THE PROJECT.

3. ONLY UPON STABILIZATION OF ALL DISTURBED AREAS MAY EROSION CONTROL DEVICES BE REMOVED. ALSO, ALL STORM SEWERS MUST BE CLEANED OF ALL SEDIMENT.

SOIL EROSION AND SEDIMENTATION CONSTRUCTION NOTES:

1. ALL SOIL EROSION CONTROL MEASURES SHALL COMPLY WITH THE CURRENT CITY OF ANN ARBOR ORDINANCES. WASHTENAW COUNTY STANDARDS AND SPECIFICATIONS FOR SOIL EROSION AND SEDIMENT CONTROL, AND STATE OF MICHIGAN "SOIL EROSION AND SEDIMENTATION CONTROL ACT" (ACT #347).

2. CONTRACTOR SHALL HAVE A PRE-GRADING MEETING WITH THE CITY OF ANN ARBOR SOIL EROSION CONTROL STAFF PRIOR TO ANY GRADING ACTVITIES.

3. THE SITE REQUIRES AN SESC PERMIT FROM THE CITY OF ANN ARBOR. INSPECTIONS WILL BE PERFORMED BY A CERTIFIED MDEQ STORM WATER OPERATOR AT LEAST ONCE A WEEK AND IMMEDIATELY FOLLOWING EACH PRECIPITATION EVENT.

4. PRIOR TO COMMENCING EARTHMOVING OPERATIONS, THE GRADING CONTRACTOR SHALL INSTALL THE MUD TRACKING MAT, THE SILT FENCE AND TEMPORARY GRAVEL FILTER(S) SHOWN ON THE PLANS.

5. ANY LAWN AREA WHICH WILL HAVE A SLOPE STEEPER OR EQUAL TO 3:1 (3 FT. MEASURED HORIZONTALLY AND 1 FT. MEASURED VERTICALLY) SHALL BE SODDED AND PEGGED OR SEEDED AND MULCHED USING A SOIL EROSION CONTROL FABRIC OR BLANKET. HYDROSEEDING MAY BE USED IN LIEU OF SEED AND MULCH OR SOD WHERE SLOPES ARE FLATTER THAN 3:1.

6. THE ACTUAL LOCATION OF THE MUD TRACKING MATS AND THE GRAVEL FILTERS MAY BE ADJUSTED BY THE CONTRACTOR TO MATCH CONTRACTOR'S OPERATIONS AND FIELD CONDITIONS BUT ONLY IF APPROVED BY THE ENGINEER.

7. ALL DISTURBED AREAS, EVEN WHERE FUTURE PAVEMENT AND BUILDINGS ARE PROPOSED, ARE TO BE REVEGETATED PER COUNTY STANDARDS FOR TEMPORARY SEEDING.

8. BOTH INTERNAL AND EXTERNAL STREETS WILL BE CLEANED OF ANY MUD IMMEDIATELY FOLLOWING EACH MUD TRACKING OCCURRENCE.

9. PERMANENT SOIL EROSION CONTROLS ARE REQUIRED TO BE INSTALLED WITHIN 5 DAYS AFTER FINAL GRADING OR FINAL EARTH CHANGE.

10. DRAINAGE FROM ALL IMPERVIOUS AREAS IS TO BE DIRECTED TO THE ON-SITE STORM WATER MANAGEMENT SYSTEM.

11. THE OBTAINING OF BUILDING PERMITS, AND BUILDING FOOTING CONSTRUCTION MAY NOT BEGIN UNTIL THE SITE STORMWATER MANAGEMENT SYSTEM IS INSTALLED AND OPERATIONAL.

12. THE ESTIMATE COST TO ESTABLISH A GRASS SEED MIX IN DISTURBED AREAS, IF CONSTRUCTION WERE TO BE DISCONTINUED, IS \$8,000, FOR TOPSOIL SPREADING, SEEDING, AND WATERING.

13. THE PROJECT WILL INVOLVE APPROXIMATELY 600 CYD OF CUT, 800 OF FILL, AND 1,900 CYD OF UTILITY TRENCH CUT AND BACKFILL. THIS NUMBER WILL VARY BASED UPON CONTRACTOR TECHNIQUES, AND ALL BIDDERS ARE REQUIRED TO PERFORM THEIR OWN EARTHWORK CALCULATIONS BEFORE BIDDING.

DURING CONSTRUCTION: TASK Inspect for sediment accumulation Removal of sediment accumulation Inspect for floatables and debris Cleaning for floatables and debris Inspect for erosion Reestablish permanent vegetation on eroded Clean drives and parking lots Water disturbed areas to provide dust control Inspect structural elements during wet weath compare to as-built plans (by a professional engineer reporting to the owner) Make adjustments or replacements as deterr by wet weather inspection * "as needed" means when sediment has acc Maintenance of soil erosion and sedimentatio PERMANENT MAINTENANCE: TASI Inspect for sediment accumulation Removal of sediment accumulation Inspect for floatables and debris Cleaning for floatables and debris Inspect for erosion Reestablish permanent vegetation on eroded Clean drives and parking lots Mowing Inspect structural elements during wet weath compare to as-built plans (by a professional engineer reporting to the owner) Make adjustments or replacements as deterr by wet weather inspection Keep records of all inspections and maintena Keep records of all costs for inspections, Property owner to review cost-effectiveness o preventative maintenance program and make necessary adjustments. Onwer to hire a professional engineer to carry emergency inspections upon identification of problems.

14. THE P	ROJECT'S DISTURBED AREA IS A	PPROXIMATELY 1.13 ACRES.		
PLYWOOD 48"X24" BLACK LETTERS PAINTED WHITE 7 6" HEIGHT				
36" WOOD POST 3.5"X3.5"X8'				
36°				
CONCRETE WASHOUT SIGN DETAIL (OR EQUIVALENT)				
STAPLE				
LE DETAIL ON PAVEMENT, DRY-LAID CONCR BLOCKS MAY BE USED INSTEAD	ETE DF		40444 40044 400444 40044 400444 40044 40044 40044 40044 40044	
TRAW BALES STRAW BALES AND STAKES	FLOW			
<u>ashout</u> e	The second			
	PUMP DISCHARGE HOSE			
			I, LEAF/WOOD COMPOST, CHIPS, SAND, OR STRAW BALES	<u>PLAN VIEW</u>
			SLOPE	SULT STOP FENCE FAE
<u>PLAN</u> 				2'-6" WIDE
		ELEVATION	FILTER BAG	
 STANDARD 48" HIGH SNOW FENCE OR ORANGE PLASTIC FENCE 	CONSTRUCTION SPECIFICATION	ONS		
	1. TIGHTLY SEAL SLEEVE AROUND TH	E PUMP DISCHARGE HOSE WITH A STR	AP OR SIMILAR DEVICE.	
	2. PLACE FILTER BAG ON SUITABLE STRAW BALES) LOCATED ON A LE STABILIZED AREA. EXTEND BASE	BASE (E.G., MULCH, LEAF/WOOD COMPO IVEL OR 5% MAXIMUM SLOPING SURFACE A MINIMUM OF 12 INCHES FROM EDGES	DST, WOODCHIPS, SAND, OR E. DISCHARGE TO A OF BAG.	
<u>ELEVATION</u> SNOW FENCE SHALL BE LOCATED AT THE OUTER PERIMETER OF THE	 CONTROL PUMPING RATE TO PREV WITH THE MANUFACTURER RECOM RATE. 	/ENT EXCESSIVE PRESSURE WITHIN THE MENDATIONS. AS THE BAG FILLS WITH S	FILTER BAG IN ACCORDANCE SEDIMENT, REDUCE PUMPING	
SPREAD OF THE BRANCHES, OR CLOSER ONLY AT THE DIRECTION OF THE ENGINEER.	 REMOVE AND PROPERLY DISPOSE AFTER BAG HAS REACHED CAPAC FROM THE BAG IN AN APPROVED OF THE WORK DAY. RESTORE THE REMOVAL OF THE DEVICE. 	OF FILTER BAG UPON COMPLETION OF ITY, WHICHEVER OCCURS FIRST. SPREAD UPLAND AREA AND STABILIZE WITH SE SURFACE AREA BENEATH THE BAG TO	PUMPING OPERATIONS OR) THE DEWATERED SEDIMENT ED AND MULCH BY THE END) ORIGINAL CONDITION UPON	FRONT VIEV UPHILL SIDE FENCE TO E COMPACTED
	 USE NONWOVEN GEOTEXTILE WITH SLEEVE TO ACCOMMODATE A MAX MANUFACTURED FROM A NONWOV VALUES (MARV) FOR THE FOLLOW 	DOUBLE STITCHED SEAMS USING HIGH (IMUM 4 INCH DIAMETER PUMP DISCHAR) EN GEOTEXTILE THAT MEETS OR EXCEED (ING:	STRENGTH THREAD. SIZE GE HOSE. THE BAG MUST BE DS MINIMUM AVERAGE ROLL	
	GRAB TENSILE PUNCTURE	250 LB 150 LB	ASTM D-4632 ASTM D-4833	
TECTION FENCE	FLOW RATE PERMITTIVITY (SEC ⁻¹) UV RESISTANCE APPARENT OPENING SIZE (AOS) SEAM STRENGTH	70 GAL/MIN/FT ² 1.2 SEC ⁻¹ 70% STRENGTH @ 500 HOURS 0.15-0.18 MM 90%	ASTM D-4491 ASTM D-4491 ASTM D-4355 ASTM D-4751 ASTM D-4632	<u>CROSS-SEC</u>
NOT TO SCALE	 REPLACE FILTER BAG IF BAG CLO CONNECTION BETWEEN PUMP HOS DISPLACED. 	GS OR HAS RIPS, TEARS, OR PUNCTURE E AND FILTER BAG WATER TIGHT. REPL/	ES. DURING OPERATION KEEP ACE BEDDING IF IT BECOMES	<u>SILT F</u>
		DEWATERING FILTER B	AG	
		NOT TO SCALE		

STORMWATER /SESC MAINTENANCE SCHEDULE RACQUET CLUB OF ANN ARBOR	E									B108
DURING CONSTRUCTION: FASK	Paved Area	s Pervious Areas	Riprap &	Storm	Catch Basins	Inlet	Flow Restriction	n Chambers a	& SCHEDULE	e gan 4
nspect for sediment accumulation	X		Silt Fence	Pipes X X	and Manholes X X	Grates	Devices X X	QC Devices	s Weekly As needed* & prior to turnover	Drive Michi 0599
Icening for floatables and debris	X			X X X	X X X	X X	X X X	X X X	Quarterly Quarterly and at tumover	SC Plaze 734.(34.995
nspect for erosion Reestablish permanent vegetation on eroded slopes Clean drives and parking lots	X	X X	X						Weekly As needed* & prior to turnover Weekly or as determined by permitting agency	Ann A Phone: Fax 7.
Nater disturbed areas to provide dust control nspect structural elements during wet weather and	X	X							As needed* & prior to turnover	
compare to as-built plans (by a professional engineer reporting to the owner) Make adjustments or replacements as determined			x	x			Х	Х	Annually and at turnover	ntal a nginee ors
by wet weather inspection "as needed" means when sediment has accumulate	ed to a minim	um of one foot dept	x h.	Х			Х	Х	As needed* & prior to turnover Total Project Phase Cost	nmen on Er Archit
Maintenance of soil erosion and sedimentation during	construction	to be the repsonsi	bility of the to	o-be-sele	ected contractor,	and ultin	nately to the deve	loper.		Enviro ortatio rs, Si
PERMANENT MAINTENANCE:										tivil, E ransp Ilanne andsc
TASK	Paved Area	s Pervious Areas	Riprap	Storm Pipes	Catch Basins and Manholes	Inlet Grates	Flow Restriction Devices	n Chambers a QC Devices	& SCHEDULE s	
nspect for sediment accumulation Removal of sediment accumulation	X X		X X	X X X	X X X	x	X X X	X X X	Annually Annually, and as needed*	
Cleaning for floatables and debris		X	X	X	X	X	X	X	Annually, and as needed* Every six months	
Reestablish permanent vegetation on eroded slopes Clean drives and parking lots	Х	X							As needed* Annually	
Nowing nspect structural elements during wet weather and compare to as-built plans (by a professional		X							Weekly during growing season	
Angineer reporting to the owner) Nake adjustments or replacements as determined			X	X			Х	X	Annually	
we weather inspection Keep records of all inspections and maintenance			X	X			Х	X	As needed* Annually	SOR
Keep records of all costs for inspections, Property owner to review cost-effectiveness of the preventative maintenance program and make									Annually	ARB
ecessary adjustments. Drwer to hire a professional engineer to carry out									Annually	ANN E 8104
emergency inspections upon identification of severe problems.									As needed*	~ 0F LAN AKER 79
"as needed" mana when addiment has a second by	ed to a minim	um of one fact days							Total Annual Cost	CLUE CLUE XORY NR, M HOM/
Permanent maintenance of soil erosion and sedimen	tation control	to be the resPonsit	nility of the R	acquet (Club of Ann Arbo	r and en	forced by the City	of Ann Arbor		ENT UET HIC ARBC T SC
PLAN VIEW				_			GRATE –	POL,	YPROPYLENE BOOT" HIGH FLOW OVERFLOW POLYPROPYLENE FILTER BAG	RACQUET CLUB OF SITE PLAN SESC NOTES AND DE
N MIN. OR ANCE DING OR MENT PON ZE ST BE OL CROSS-SECTIO SILT FEN MES 2'-6" WIDE TOR TOR TOR TOR TOR TOR TOR T		$\frac{2^{n}x}{1^{n}-6^{n}}$	2" STAKES "INTO GR		N <u>INS</u>	TALLA	TION DETA TO STRAP – TO STRAP – TION DETA DUMP STRAP – TREBAR FOR REMOVAL FROM SILTSACK –	ART INLET S ED ON ALL I INLETS. INL REAMGUARD" (ATER SERVIC TSACK" AS N UCTION FABF FILTER AS N ALL BAG MINLET ENGTH=L	SEDIMENT FILTER TO BE PAVED CATCH BASINS OR ET FILTER TO BE SIMILAR AS MANUFACTURED BY CES CORPORATION (206–767–0441) MANUFACTURED BY ATLANTIC RICS, INC.; (800–448–3636). EEDED. 2 EACH DUMP STRAPS EXPANSION RESTRAINT (1/4" NYLON ROPE. 2" FLAT WASHERS) BAG DETAIL MIDTH=W (INLET FILTER) SCALE	14058 Date: 5/15/2015 Rev. Date Date: 5/15/2015 Rev. Date CadD: WaJ Rev. Date CadD: WaJ PM: SWB PM: SWB PM: SWB PM: SWB 14058DT1.dwg
KEEP OMES <u>SILT FEN</u>	<u>NCE [</u> no scale	Detail					<u>SILT S</u>	SACK NO	(INLET FILTER) scale	OB No. 1405 EVISIONS:

(3d_Proj\14058\Site Plan\14058DT1.dwg, 13.1, 5/14/2015 4:30:19 PM, JAM, DWG to PDF.pc3

-6"-10" NOTCHES CUT IN SHADED AREAS

R-TANKHD_ TYPICAL MAINTENANCE PORT

FABRIC PIPE BOOT FOR R-TANKHD

STRUCTURE R-36: CDS3030-6-C (OR ENGINEER APPROVED EQUAL) 2.8 MIN. CFS RATED CAPACITY - 10.0 CFS BYPASS CAPACITY

DIMENSIONS AND WEIGHTS, PLEASE CONTACT YOUR CONTECH

4. CDS WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS

5. STRUCTURE SHALL MEET AASHTO HS20 AND CASTINGS SHALL GROUNDWATER ELEVATION AT, OR BELOW, THE OUTLET PIPE

6. PVC HYDRAULIC SHEAR PLATE IS PLACED ON SHELF AT BOTTOM

OF SCREEN CYLINDER. REMOVE AND REPLACE AS NECESSARY

PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND LIFTING AND REACH CAPACITY TO LIFT AND SET THE CDS

D. CONTRACTOR TO PROVIDE, INSTALL, AND GROUT PIPES. MATCH E. CONTRACTOR TO TAKE APPROPRIATE MEASURES TO ASSURE UNIT IS WATER TIGHT, HOLDING WATER TO FLOWLINE INVERT MINIMUM. IT IS SUGGESTED THAT ALL JOINTS BELOW PIPE

HYDRODYNAMIC SEPARATOR GENERAL NOTES (CONSTRUCT CDS OR ENGINEER-APPROVED EQUAL IN ACCORDANCE WITH ALL MANUFACTURER INSTRUCTIONS.)

MIDWFSTERN CONSIII TING	Civil, Environmental and 3815 Plaza Drive	Transportation Engineers Ann Arbor, Michigan 48108 Planners, Surveyors Phone: 734.995.0200 Landscape Architects Fax 734.995.0599
CLIENT	RACQUET CLUB OF ANN ARBOR 3010 HICKORY LANE	ANN ARBOR, MI 48104 BRENT SCHOMAKER (734) 216-0579
RACOUFT CLUR OF ANN ARROR		STORMWATER QUALITY DEVICE DETAILS
	2	0
DATE: 5/15/2015 SHEET 20 OF 22	REV. DATE CADD: WAJ	ENG: JAM PM: SWB TECH: 14058DT1.dwg
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